

*Kindly replace Paragraph 0010 with the following:*

Q2  
Preferred embodiments of the invention are disclosed in the following description and illustrated in the accompanying drawings, in which:

sub B2  
Fig. 1 shows a standard schematic illustration of the actually known 450° transposition according to *Willyoung* of a stator winding bar with 2 x 6 shrouds and the surfaces of two selected shrouds, which are effective for the external field, with the plus or minus signs that are important for the summation of the loop currents (the surfaces or respectively external field portions in the end windings are not compensated);

Fig. 2 shows the situation of the stator bar in Fig. 1 in relation to the inherent field;

Fig. 3 shows an illustration of an exemplary embodiment of a stator bar according to the invention, with extended middle part and resulting compensation of the external field portions in the end windings;

Fig. 4 shows the situation of the stator bar in Fig. 3 in relation to the inherent field;  
and,

Fig. 5 shows a comparison of the amplitudes of the shroud currents in relation to the nominal value for the example of a stator winding bar with standard 450° transposition (graph a) and transposition according to the invention (graph b).

*Kindly replace Paragraph 0011 with the following:*

Q3  
sub B3  
Fig. 1 to 4 each show a side view of a stator winding bar 10 (Roebel bar) with a total of  $2 \times 6 = 12$  shrouds 11,...,14. The stator winding bar 10 is positioned with an active part AT in the winding slot of the stator laminated core. Within the active part, the shrouds 11,...,14

*A3  
should  
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B3  
concl'd*

undergo a transposition of  $450^\circ$ . End winding WK, in which the shrouds 11,...,14 are not transposed, border the active part AT on both sides. The active part AT is divided into a middle part MT and two border zones RZ of equal length that enclose the center part MT. In the center part, the transposition is  $270^\circ$ , in the border zones RZ  $90^\circ$  each.

*Kindly replace Paragraph 0013 with the following:*

*A4  
SUB  
B4*

Reference number 11 stands for the 6 shrouds of the rear stack (in viewing direction); reference number 12 stand for the front stack. When the shrouds are located in the front during the transposition, they are drawn with continuous lines; when they are in the back, they are drawn with broken lines. A representative loop with shrouds 13 and 14 is in each case drawn with a thick line and is used to evaluate the transposition, whereby the plus or minus signs essential for the compensation are in each case entered. Two evaluations are made: first the external field analysis in Fig. 1 or Fig. 3 (surfaces within the loops must be added with the respective, correct plus or minus signs), and then the inherent field analysis in Fig. 2 or Fig. 4 (surfaces within the loops in relation to the center line 15 of the winding bar must be added with the respective, correct plus or minus signs). If the sum of all partial surfaces is zero, no circulating currents occur.

*Kindly replace Paragraph 0014 with the following:*

*A5  
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B5*

As can be clearly seen from Fig. 1, the external field portions in the end windings WK, which penetrate the loop (drawn with thick line) of shrouds 13 and 14, are not

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cancel.*

compensated during the standard transposition. In contrast, the external field portions in the active part AT are all compensated.

*Kindly replace Paragraph 0016 with the following:*

*A6  
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D6  
cancel.*

According to the invention, the formula of *Willyoung* regarding the length of the middle part MT for the 450° transposition is now changed to the effect that this section is extended beyond 3/4 of the length of the active part AT (the middle part MT still has a 270° transposition). In this way, the shrouds that carry most of the current, are kept near the slot bottom for a longer distance, and those that carry the least current are kept for a longer distance in the active part AT towards the slot opening. It is known that these conditions have a compensating effect on the current distribution in the Roebel bar. This transposition can be described as (0/450unv/0) (unv = incompletely compensated in active part, in order to compensate the residual field of the end winding).

*Kindly replace Paragraph 0017 with the following:*

*A7  
SUB  
D6  
cancel.*

According to Fig. 3, in such a stator winding bar with 450° transposition in the extended active part AT, the external field portions in the end windings WK that penetrate the loop (shown bold) of the shrouds 13 and 14, are compensated by the cross-wise striated (additional) portions in the active part AT. The extension of the middle part MT is hereby preferably chosen so that a maximum compensation is achieved. The residual external field portions in the active part AT are all compensated.